

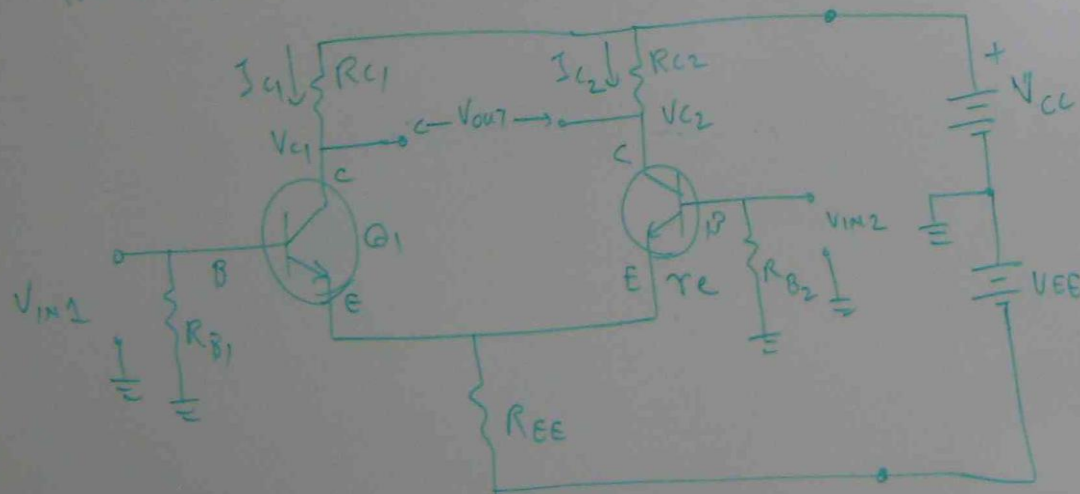
UEENEE H029 B

PROVIDE SOLUTION TO ϕ ELECTRONICS POWER CONTROL PROBLEMS

+ 82732 VARIABLE SPEED DRIVES

DC CONDITION OF DIFFERENTIAL AMPLIFIER

THE DIFFERENTIAL AMPLIFIER IS A DC COUPLED AMPLIFIER THAT AMPLIFIES THE DIFFERENCE BETWEEN TWO INPUT VOLTAGES V_{IN1} AND V_{IN2}



THE DIFFERENTIAL AMPLIFIER

$V_{BE} = 0.6V$ FOR SILICON TRANSISTOR

$$I_{EE} = \frac{V_{R_{EE}}}{R_{EE}}$$

$$I_{C1} = I_{C2} = \frac{I_{EE}}{2}$$

$$V_C = V_{CC} - I_C R_C$$

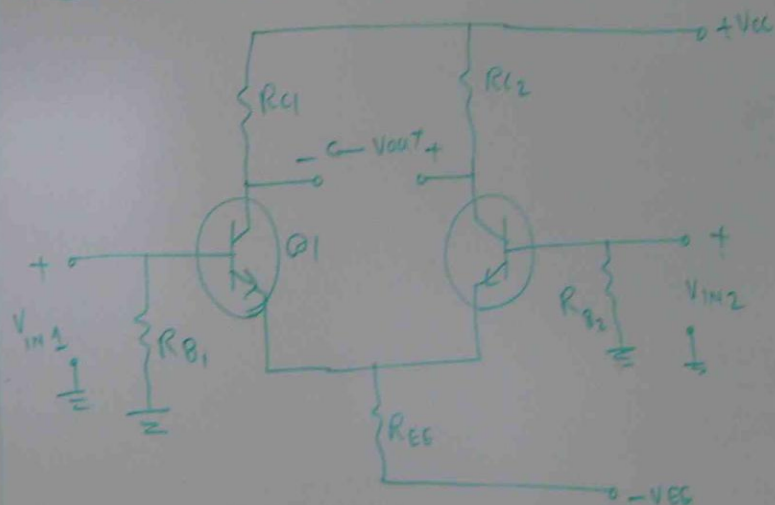
$$V_{C1} = V_{CC} - I_{C1} R_{C1}$$

$$V_{C2} = V_{CC} - I_{C2} R_{C2}$$

DIFFERENTIAL VOLTAGE GAIN (A_d)

$$A_d = \frac{R_C}{2r_e} \quad r_e = \frac{30\text{mV}}{I_E}$$

VOLTAGE GAIN FOR THE BALANCED INPUT, BALANCED OUTPUT
DIFFERENTIAL AMPLIFIER

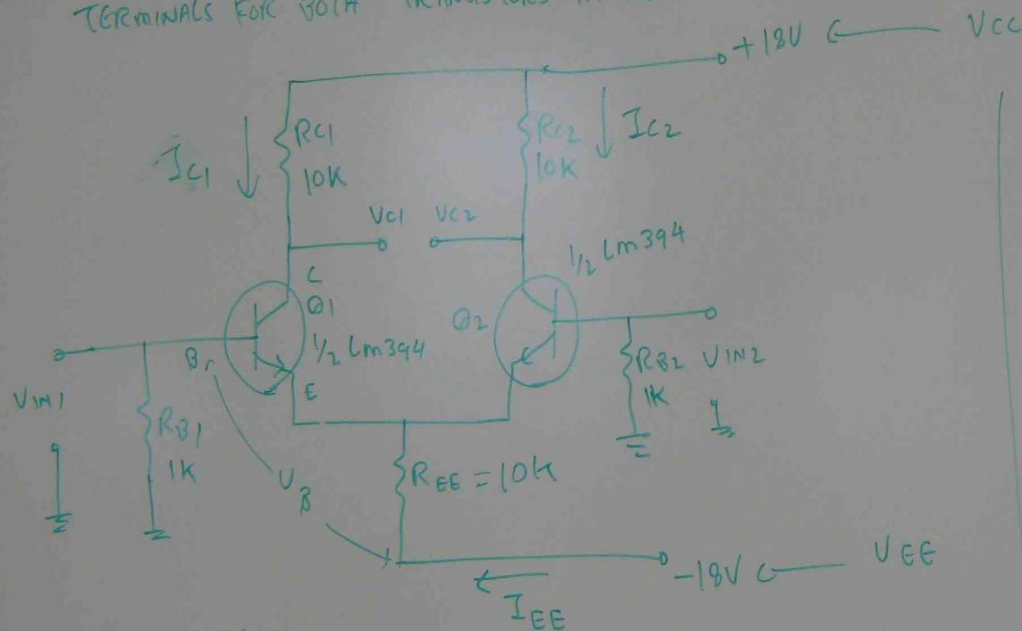


$$V_d = V_{IN1} - V_{IN2}$$

$$A_d = \frac{R_C}{r_e}$$

$$r_{in} = 2\beta r_e$$

pb DETERMINE THE VOLTAGES PRESENT AT THE BASE, COLLECTOR AND EMITTER TERMINALS FOR BOTH TRANSISTORS IN THE CIRCUIT.



$$I_{EE} = \frac{V_{EE}}{R_{EE}} = \frac{18}{10k} = 1.8 \text{ mA}$$

$$I_{C1} = I_{C2} = \frac{I_{EE}}{2} = \frac{1.8}{2} = 0.9 \text{ mA}$$

$$V_{C1} = V_{CC} - I_{C1} R_{C1}$$

$$= 18 - 0.9 \times 10^{-3} \times 10 \times 10^3$$

$$= 18 - 9$$

$$= 9 \text{ V}$$

$$V_{C2} = 9 \text{ V}$$

$$V_B = V_{BE} + I_{EE} \times R_{EE}$$

$$= 0.6 + 1.8 \times 10^{-3} \times 10 \times 10^3$$

$$= 18.6 \text{ V}$$

COLLECTOR AND EMITTER

18V \leftarrow V_{CC}

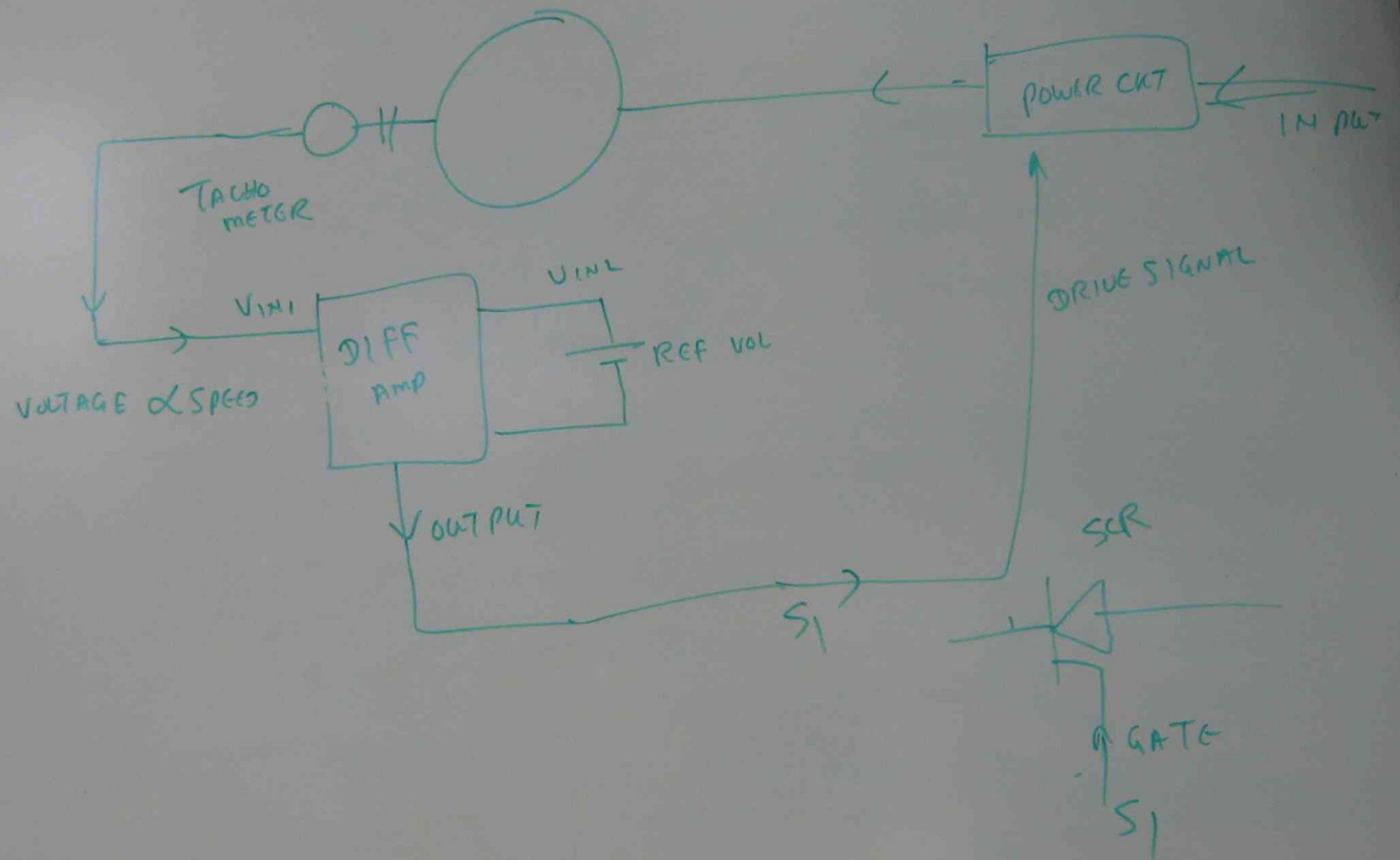
$$\begin{aligned} V_C &= V_{CC} - I_{C1} R_{C1} \\ &= 18 - 0.9 \times 10^{-3} \times 10 \times 10^3 \\ &= 18 - 9 \\ &= 9V \end{aligned}$$

V_{EE}

$$V_{C2} = 9V$$

$$\begin{aligned} V_B &= V_{BE} + I_{EE} \times R_{EE} \\ &= 0.6 + 1.8 \times 10^{-3} \times 10 \times 10^3 \\ &= 18.6V \end{aligned}$$

$$\begin{aligned} V_E &= I_{EE} \times R_{EE} \\ &= 1.8 \times 10^{-3} \times 10 \times 10^3 \\ &= 18V \end{aligned}$$



NOISE REJECTION AND INTRODUCTION TO THE OPERATIONAL AMPLIFIER

DIFFERENTIAL AMPLIFIER CAN REJECT THE NOISE SIGNALS THAT ARE
COMMON TO BOTH INPUTS.

COMMON MODE REJECTION \rightarrow HOW MUCH OF COMMON MODE SIGNAL IS
PRESENT IN THE OUTPUT OF THE AMPLIFIER
IT SHOULD BE IDEALLY ZERO

$$CMRR = \frac{A_d}{A_{cm}}$$

CMRR - COMMON MODE REJECTION RATIO

A_d - DIFFERENTIAL AMPLIFIER GAIN

A_{cm} - COMMON MODE GAIN.

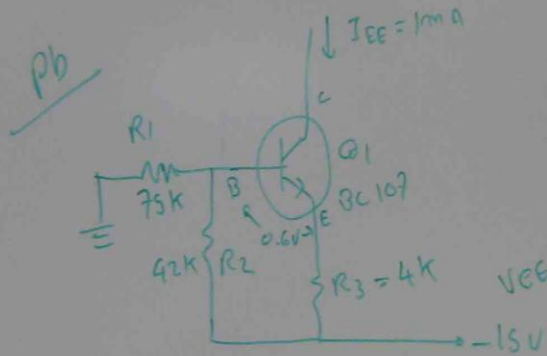
THE DISCRETE COMPONENT OF BJT CONSTANT CURRENT SOURCE



BIPOLAR JUNCTION TRANSISTOR



FIELD EFFECT TRANSISTOR FET



CALCULATE (a) V_{R2} , (b) V_{R3}
(c) I_C

$$V_{R2} = \frac{R_2}{R_1 + R_2} \times V_{EE}$$

$$V_{R3} = V_{R2} - 0.6 \text{ V}$$

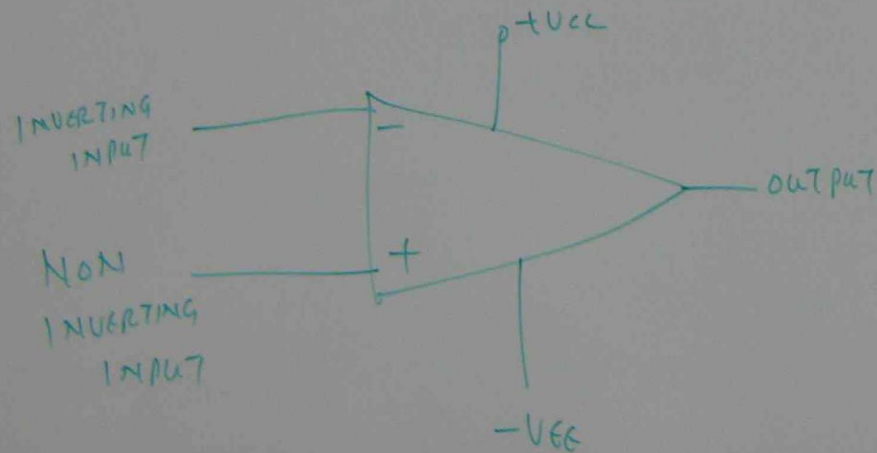
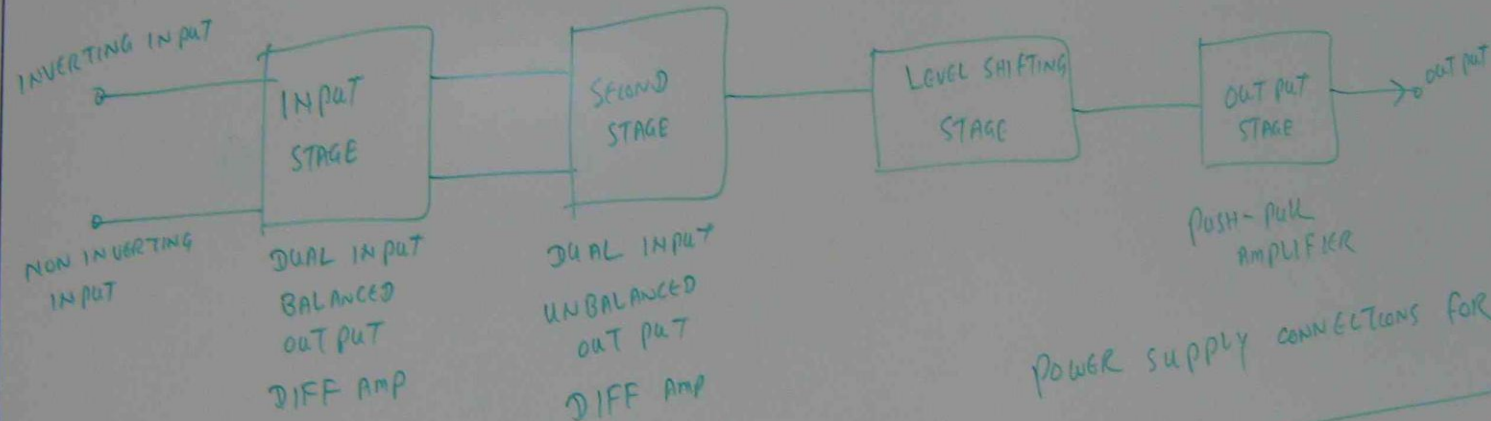
$$I_C = I_{EE} = \frac{V_{R3}}{R_3}$$

$$\begin{aligned} V_{R2} &= \frac{R_2}{R_1 + R_2} V_{EE} \\ &= \frac{42}{75 + 42} \times 15 \\ &= 5.38 \text{ V} \end{aligned}$$

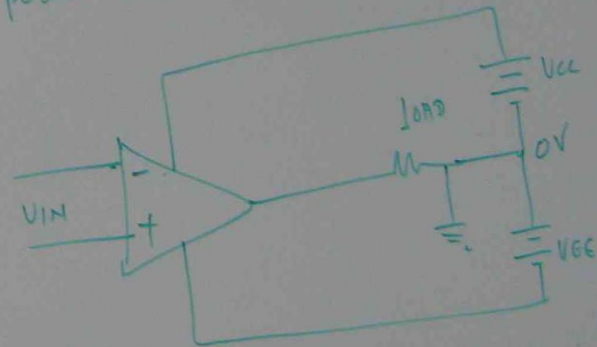
$$V_{R3} = V_{R2} - 0.6 = 5.38 - 0.6 = 4.78 \text{ V}$$

$$I_C = I_{EE} = \frac{V_{R3}}{R_3} = \frac{4.78}{4} = 1.195 \text{ mA}$$

INTRODUCTION TO THE OPERATIONAL AMPLIFIER

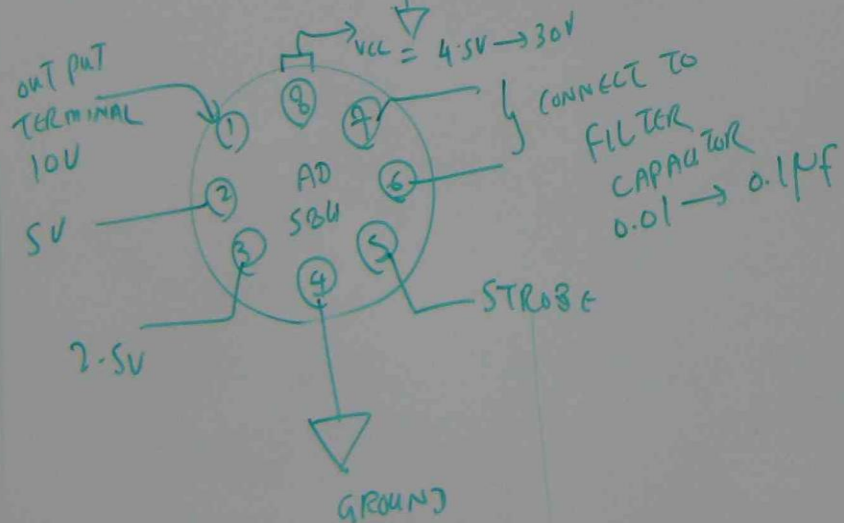
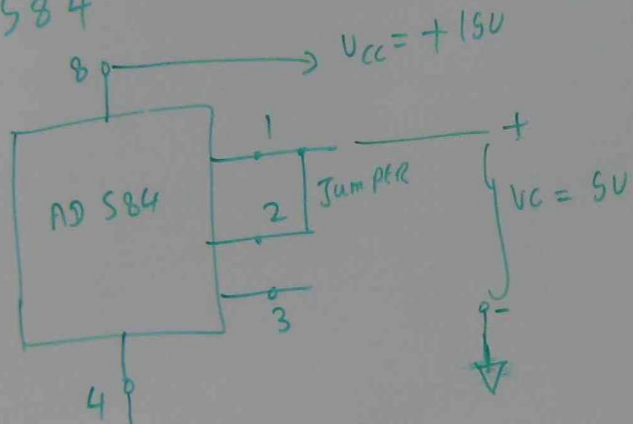


POWER SUPPLY CONNECTIONS FOR OP-AMP

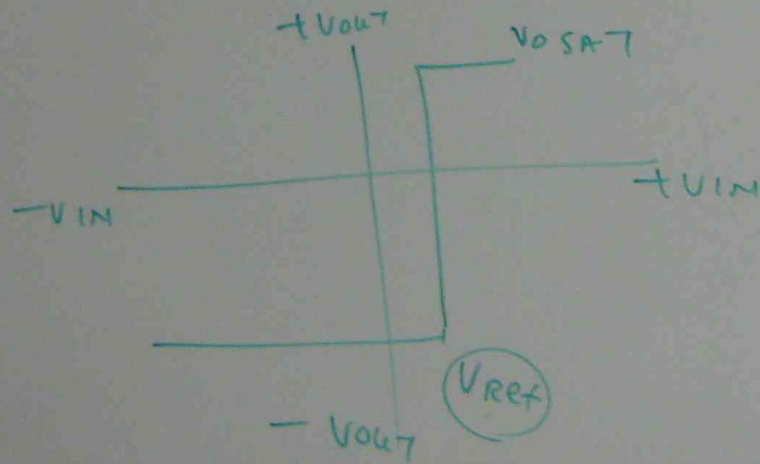
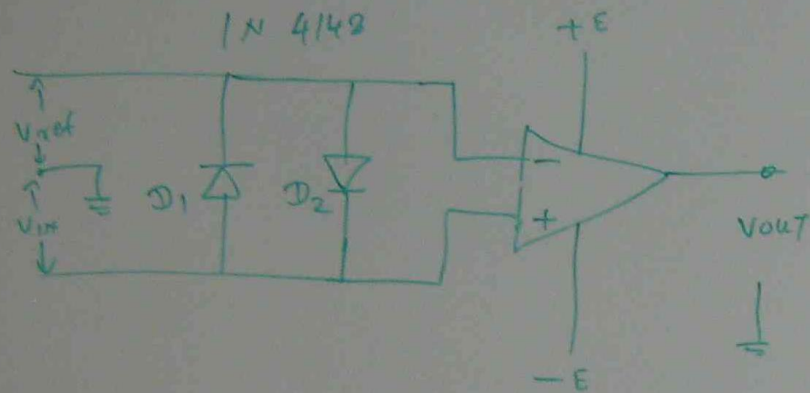


COMPARATORS

A D 584



BASIC NON INVERTING COMPARATOR CIRCUIT

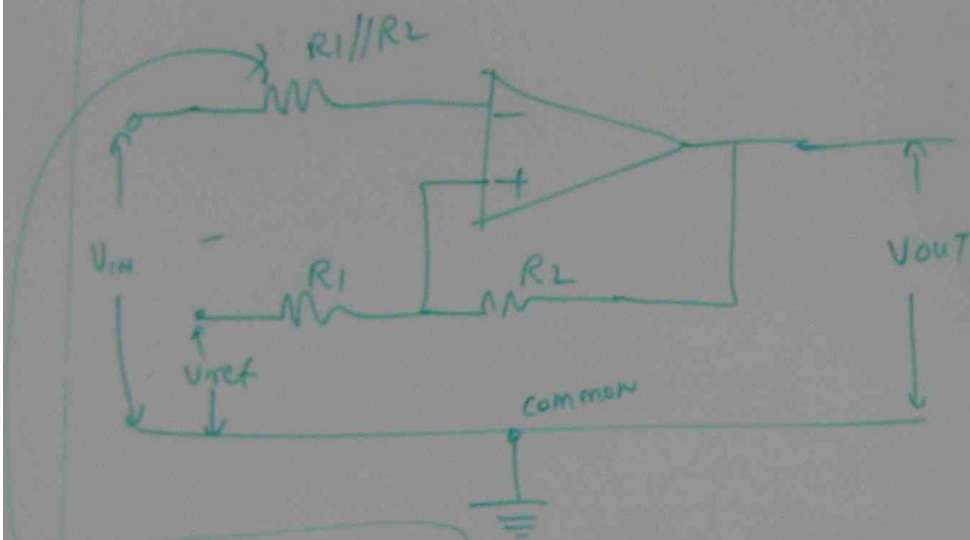


OPEN LOOP VOLTAGE GAIN (V_{IN})

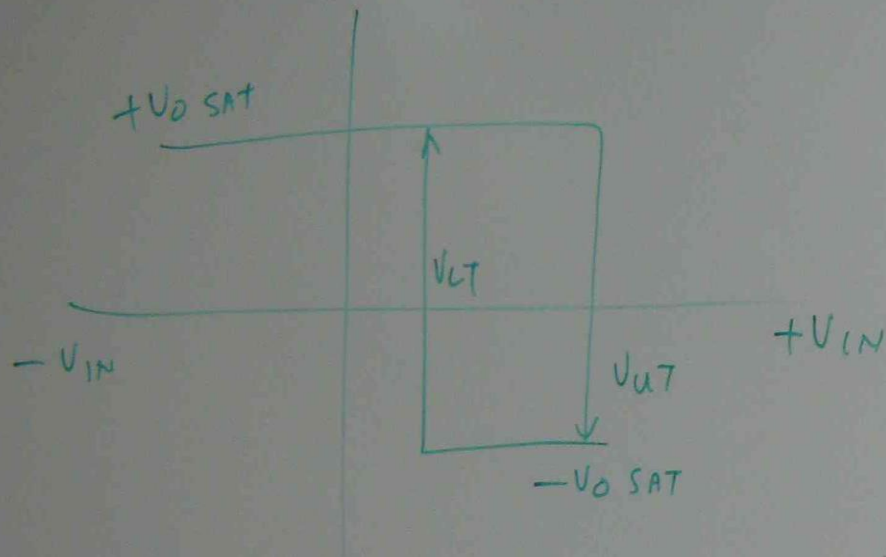
$$V_{IN} = V_{ref} \pm \frac{2 V_O (SAT)}{A_{VOL}} = V_{ref} \pm \frac{30V}{200,000}$$
$$= V_{ref} \pm 150 \mu V$$

THE DIFFERENTIAL COMPARATOR WITH VOLTAGE HYSTERESIS

INVERTING COMPARATOR WITH POSITIVE FEED BACK



$$\frac{1}{R_1 // R_2} = \frac{1}{R_1} + \frac{1}{R_2}$$

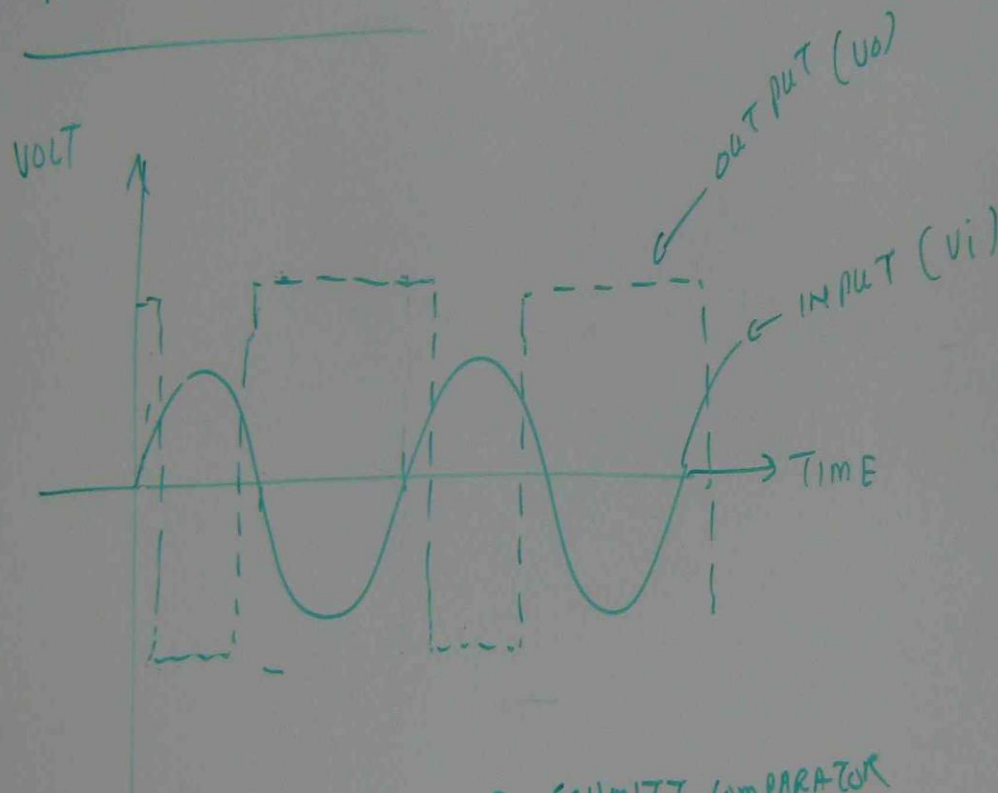


$$V_{UT} = \text{UPPER THRESHOLD VOLTAGE} = V_{ref} + \left[1 + \frac{V_{O(SAT)}}{V_{ref}} \right] \times \frac{R_1}{R_1 + R_2}$$

$$V_{LT} = \text{LOWER THRESHOLD VOLTAGE} = V_{ref} + \left[\left\{ -V_{O(SAT)} - V_{ref} \right\} \times \frac{R_1}{R_1 + R_2} \right]$$

$$V_H = \text{HYSTERESIS VOLTAGE} = V_{UT} - V_{LT}$$

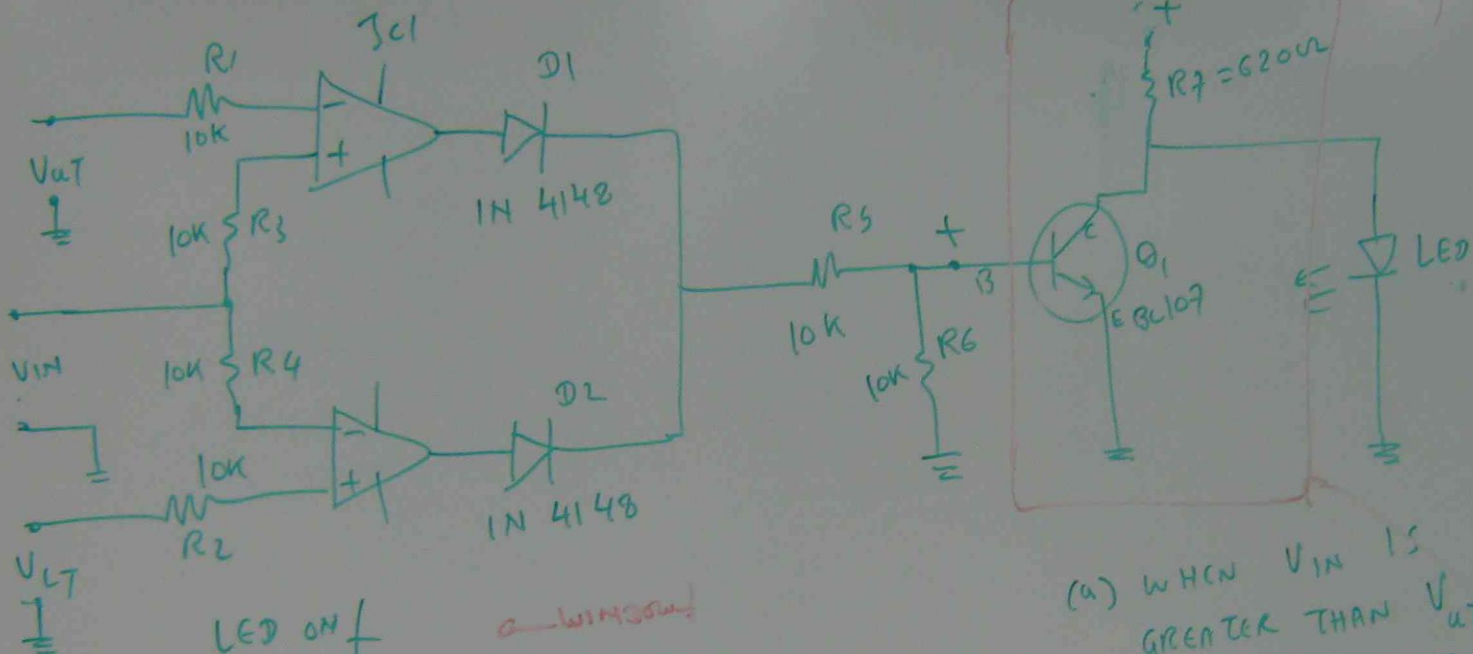
A SINE WAVE INPUT



OUT PUT WAVE FORM OF SCHMITT COMPARATOR

THE WINDOW COMPARATOR

A WINDOW COMPARATOR
WILL DETECT WHEN AN
INPUT VOLTAGE IS BETWEEN
TWO SET LEVELS.

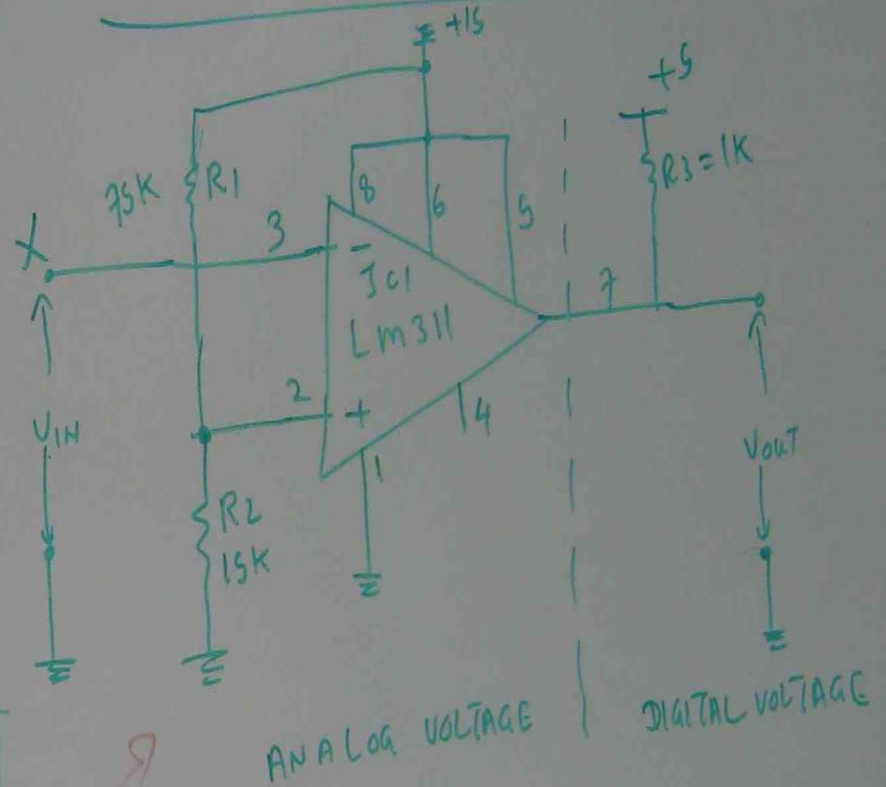


(a) WHEN V_{IN} IS GREATER THAN V_{UT} THE OUTPUT OF I_{C1} IS HIGH Q_1 IS ON THE LED IS OFF

(b) WHEN V_{IN} IS LESS THAN V_{LT} , THE OUTPUT OF I_{C2} IS HIGH, Q_1 IS ON LED IS OFF

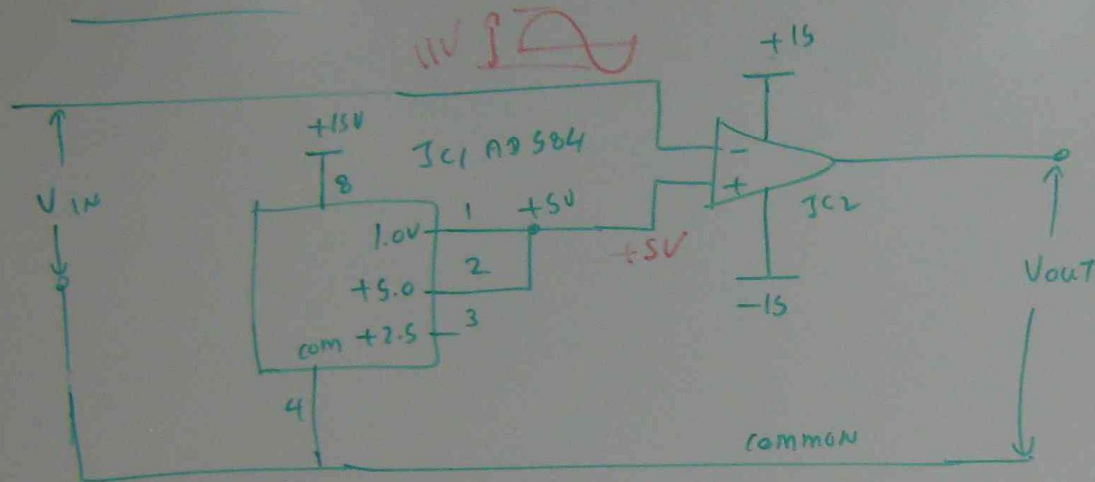
(c) WHEN V_{IN} IS GREATER THAN V_{LT} AND LESS THAN V_{UT} , THE OUT PUT OF I_{C1} AND I_{C2} WILL BE LOW CAUSING Q_1 TO TURN OFF, ALLOWING LED TO OPERATE.

INTERFACING TO DIGITAL LOGIC



EXERCISE

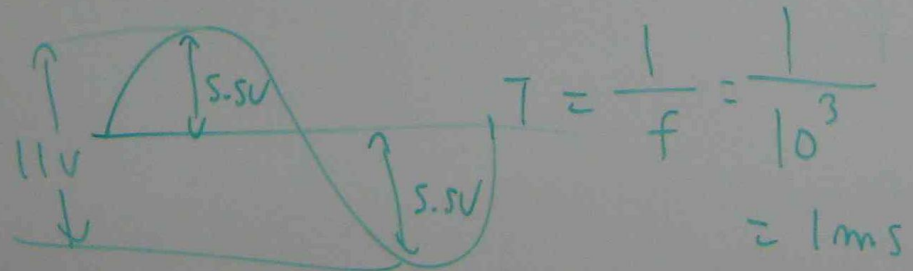
①



②

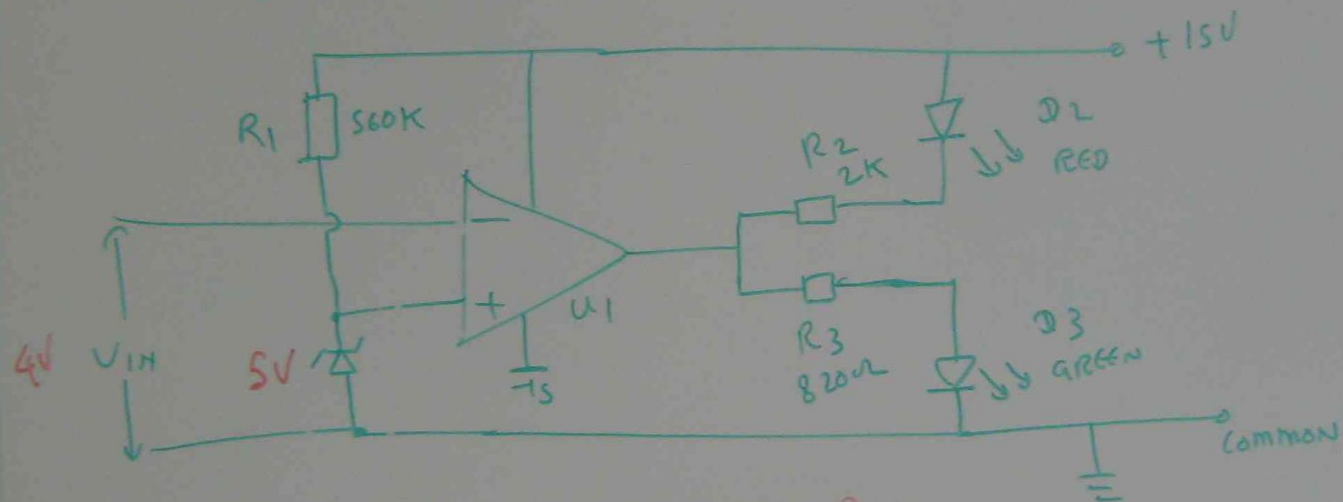
FOR THE ABOVE CIRCUIT, SKETCH THE INPUT AND OUTPUT WAVE FORMS ON A COMMON TIME SCALE IF $11V_{P-P}$, $1KHz$ SINE WAVE IS APPLIED

TO INPUT



② FOR THE CIRCUIT IN FIGURE, IDENTIFY WHICH LED IS ON UNDER THE FOLLOWING CONDITIONS.

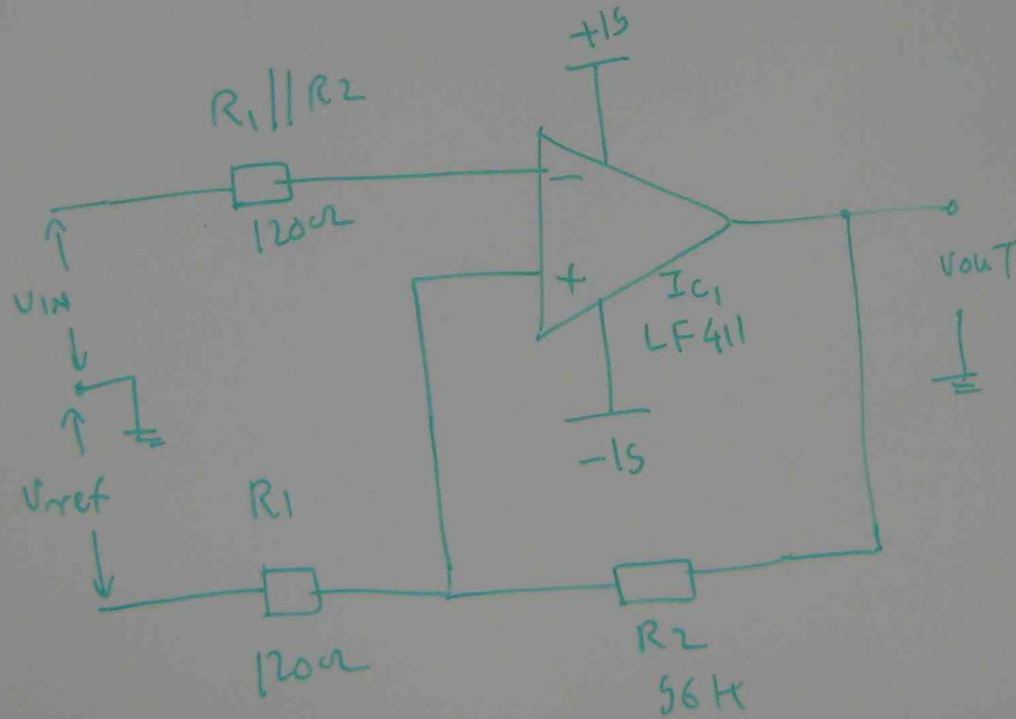
(a) IF $V_{IN} = 4V$ (b) IF $V_{IN} = 8V$



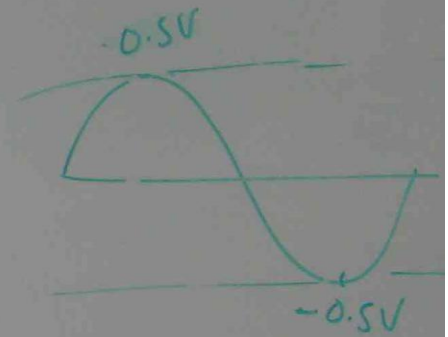
(a) D_3 (b) D_2

③ THE CIRCUIT OF THE FIGURE IS A SCHMITT TRIGGER WITH V_{ref} SET TO 0 V.

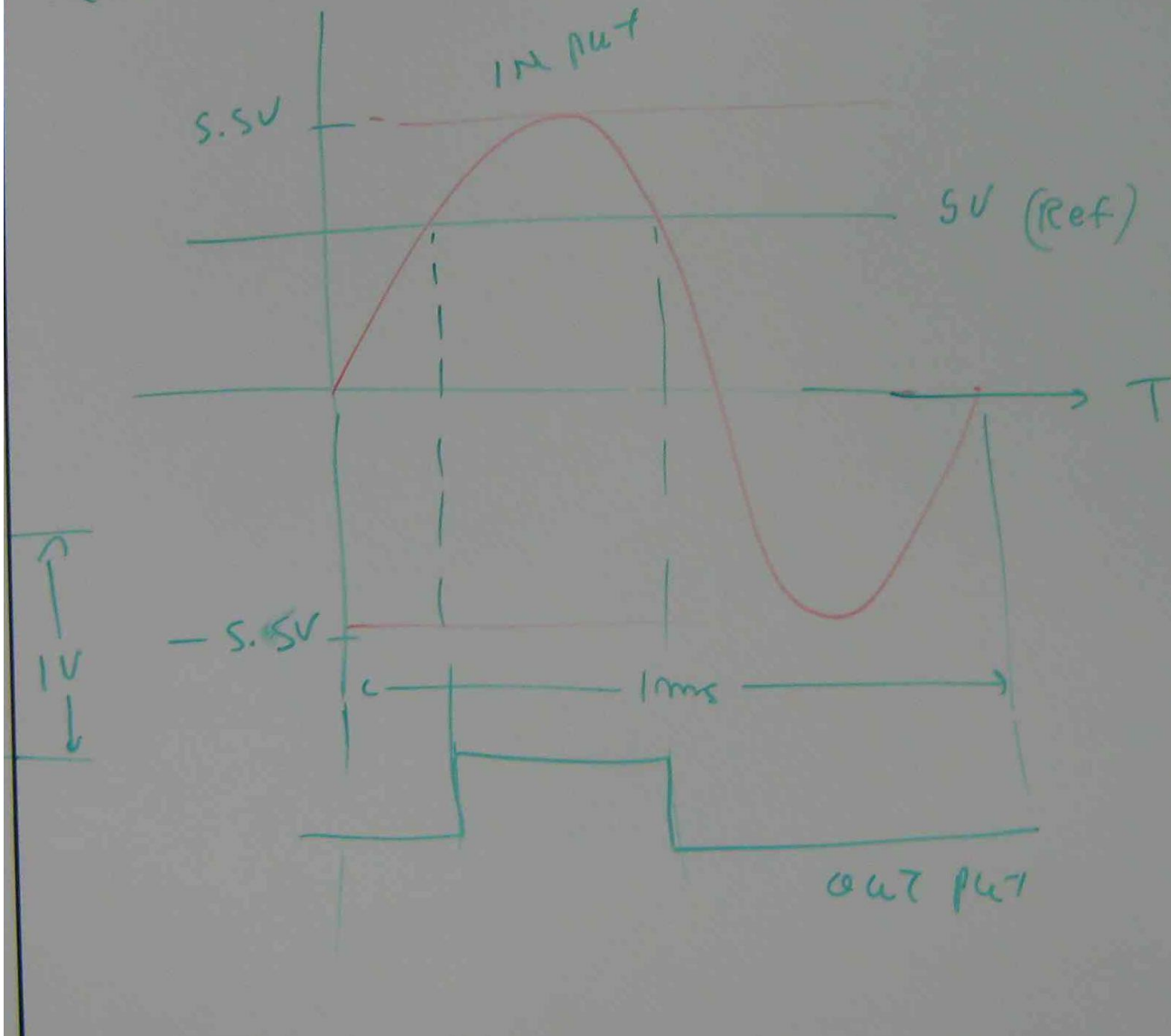
CALCULATE THE UPPER AND LOWER THRESHOLD VOLTAGES AT WHICH SWITCHING WILL OCCUR



$$V_{in} = 1 \text{ V p-p}$$



(1)



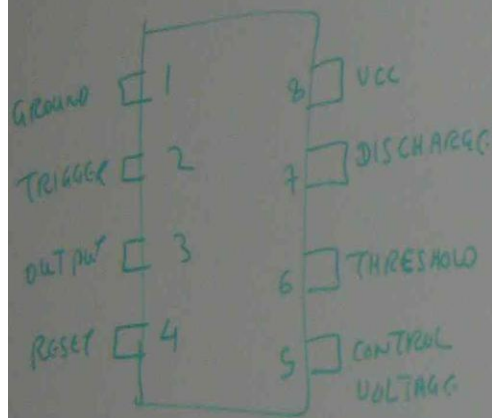
$$(3) \quad V_{uT} = V_{ref} + \left[(V_{o(SAT)} - V_{ref}) \times \frac{R_1}{R_1 + R_2} \right]$$

$$V_{LT} = V_{ref} + \left[(-V_{o(SAT)}) - V_{ref} \right] \times \frac{R_1}{R_1 + R_2}$$

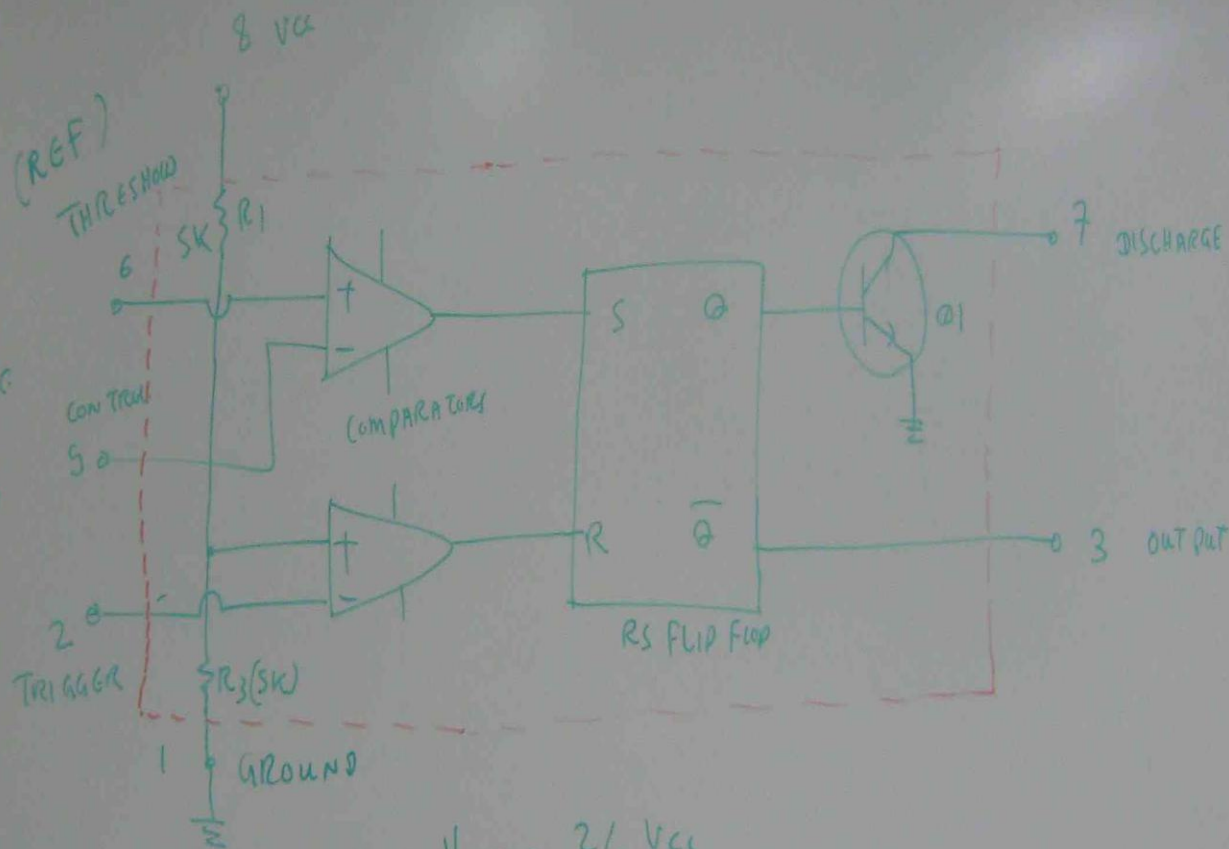
$$V_{uT} = 0 + \left[(0.5 - 0) \times \frac{120}{120 + 56 \times 10^3} \right] = 0.5 \times \frac{120}{56120} = 1.07 \text{ mV}$$

$$V_{LT} = 0 + \left[\{ -(-0.5) - 0 \} \times \frac{120}{120 + 56 \times 10^3} \right] = 0.5 \times \frac{120}{56120} = 1.07 \text{ mV}$$

TIMER 1CS



555



$$V_{UT} = \frac{2}{3} V_{CC}$$

$$V_{LT} = \frac{1}{3} V_{CC}$$